

COMPENSATING FOR POLARISATION MODE DISPERSION IN OPTICAL TRANSMISSION FIBRES

Field of the Invention

The invention relates to a technique for compensating for polarisation mode dispersion in optical transmission fibres. The invention also includes an optical transmission fibre incorporating means to compensate for polarisation mode dispersion. The invention further relates to an optical signal when subjected to such a fibre and to an equaliser for effecting such compensation.

Background to the Invention

Optical transmission fibres for use in optical transmission systems typically comprise a protective jacket surrounding a lower index cladding material enclosing a higher index optical transmission medium capable of supporting optical transmission along its length with little or no signal loss. Light is confined in the core region within such conventional step index fibres by total internal reflection as a result of the step difference in refractive index between the core and the cladding. The fibre and its cladding are near perfect circles in cross-section.

However, manufacturing tolerances, conditions of use, environmental factors and so on, give rise to imperfections in the geometric circularity of the fibres. This creates birefringence in the fibre, resulting in orthogonal polarisation states travelling at different group velocities within the fibre. Over long distances, the delay can be sufficiently cumulative that the original optical signal is effectively scrambled. This type of distortion, where orthogonal polarisation states travel at different group velocities, is known as polarisation mode dispersion (PMD).

Previous attempts at overcoming or compensating for PMD have employed either or both electrical and optical compensation techniques. Electrically based approaches are constrained to operate after the optical signal has been processed through an optical receiver (post-receiver) and are dependent on the speed of the electronics. Such electrical approaches have been found to be unsuitable for long-haul fibre links.

Optical PMD compensation techniques tend to focus on splitting the orthogonal polarisation states and delaying one relative to the other using free space optics or other optical components or, alternatively, writing a non-linear grating onto a high

birefringence optical fibre. This latter approach has met with some success. The present invention aims to improve PMD compensation.

Summary of the Invention

According to a first aspect of the invention, a method for compensating for polarisation mode dispersion in a birefringent optical transmission fibre, comprises
5 controlling the birefringence of the fibre.

In a second aspect, the invention comprises a birefringent optical transmission fibre and means for controlling the birefringence of said fibre, whereby to compensate for polarisation mode dispersion in said fibre.

10 Polarisation mode dispersion control is preferably effected by writing a non-linear fibre grating in the fibre whereby to provide a means for imposing a differential time delay to the orthogonal polarisation states arising from the effects of polarisation mode dispersion such as to compensate for said polarisation mode dispersion.

The birefringence may be imposed in the fibre by a selection of any of the
15 following options, namely introducing correctly positioned holes in the fibre so as to create a side hole fibre (SHF), a holey fibre (HF), a photonic crystal fibre (PCF) or any other suitable microstructure fibre.

The fibre grating is preferably a chirp or apodisation type grating or may be of any other suitable design. Variations in the properties of the birefringence and/or the
20 grating are preferably performed by mechanical, electrical, thermal or acoustic means or methods.

The fibre can be tapered over part or all of its length. The micro-holes in the fibre may be filled with thermally sensitive material to create stressing rods in order to impose a mechanical stress by which to control birefringence. A thermal gradient can
25 be provided over all or part of the length of the fibre. The fibre can be constructed in such a way that the fundamental transmission mode interacts with any in-fill material in the micro-holes so as to induce electro- or thermo-optic effects or voltage induced refractive index changes, or similar refractive index altering effect, in either or both of the fibre or the in-fill material that can be utilised to alter the mode shape and, consequently, the birefringence of the fibre. Any combination of these forms of fibre construction and birefringence control can be used in accordance with the invention.
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Control of birefringence can be enhanced by providing additional means, such as stress rods, to alter the stress within the fibre and thereby the modal field pattern and therefore the birefringence of the fibre.

Brief Description of the Drawings

5 The invention will now be described with reference to the following drawings, in which:

Figure 1 is a schematic representation of a cross-section through a micro-structured optical fibre;

10 Figure 2 is a graph representing the effects of polarisation mode dispersion on the group velocity of the different polarisation states;

Figure 3 is a perspective view of a tapered fibre;

Figure 4 is a side elevation of a tapered fibre with spaced heating elements; and

Figure 5 is a schematic representation of a control system for the fibre.

15 Detailed Description of the Illustrated Embodiments

As already mentioned, polarisation mode dispersion arises from the different group velocities attained by orthogonal polarisation states arising from non-perfect circularity of the fibre cross-section and hence birefringence of the fibre. The present invention takes advantage of the effects of birefringence to compensate for the polarisation mode dispersion. It is therefore an advantage to the invention, but not a necessity, to use a fibre having an inherently high birefringence at the outset.

It is known that PCF and HF fibres are highly elliptical in cross section as a result of asymmetries introduced in the manufacturing process. This gives the fibres a higher inherent birefringence than in alternative so-called high birefringence fibres.

25 PCF/HF fibres are made using a variety of techniques, primarily by systematically reducing a pre-form in size to form the geometrically micro-structured optical fibre. For example, the pre-form can be created by micro-drilling an optical pre-form or by bundling capillaries into the required geometry. The resultant micro-structured fibre often consists of a geometrical tiled pattern of air holes introduced along the length of

30 the host material. The fibre may be single material but it is not essential to the invention since a mixture of materials could still give the required birefringence, so long as the individual strands making up the fibre are correctly positioned geometrically.

The fibre may also be created in a similar drawing process but where the pre-form is made from more than one material or doped materials. In this manner the resultant fibre is still micro-structured but does not contain air holes. The materials chosen may be responsive to various optical effects, thermo-, electro-optic for example as outlined elsewhere in the present specification, allowing control over the birefringence of the fibre.

Figure 1 Illustrates schematically a cross section through a highly birefringent optical fibre. It consists of a core 1 of silica or other suitable material in which a plurality of micro-holes 2, 3 are formed by any of the techniques mentioned above. A central core region 4 with no air holes results. The refractive index of this region is considerably increased relative to the surrounding area. This core region supports optical transmission by total internal reflection of light propagating in the fibre. The surrounding material containing the micro-holes constitutes a holey cladding round the central core region. A solid silica jacket 5 is provided around the core material 1 for protection.

Figure 2 is a graph representing the effects of polarisation mode dispersion on the group velocity of the two orthogonal polarisation states in an optical fibre. The incoming signal has polarisation components along both the fibre's fast and slow axes, as indicated by the solid line 20 and the dotted line 21 respectively. The graph shows the differential time delay between the fast axis and the slow axis being Δt_1 . As discussed above, this differential delay contributes to distortion in the signal propagated in the fibre.

Fibre gratings, such as fibre Bragg gratings (FBG) are known to introduce a time delay in the signal subjected to the effects of the grating. The amount of delay can be controlled by varying certain parameters of the grating, for example by adjusting the pitch of the grating by mechanical stretching. Referring again to Figure 2, the fibre is assumed to include a grating, such as a FBG. When the grating is stretched, in the direction indicated by the arrow, the effect is to shift the curves 20, 21 to the new positions 22, 23 respectively. For any given wavelength λ_i , the time differential can be seen to have increased to the value Δt_2 , which is greater than the previous value Δt_1 . By tailoring the amount by which the grating can be used to ad-

just the differential time delay between the polarisation states, the polarisation mode dispersion can be substantially completely compensated.

Stress rods may therefore be added to the construction of the fibre to permit the characteristics of the grating to be controlled, thereby changing the modal field pattern within the core and consequently the birefringence of the fibre. This control
5 can be additional to any other means for varying the characteristics of the grating.

Convenient techniques for altering the parameters of the grating include mechanical, electrical, thermal and acoustic means and methods, as well known in the art. To be more specific, stress rods can be incorporated into the fibre such that the
10 application of a mechanical force is transferred to the grating to alter its pitch, for example. Spaced or continuous heating element(s) can be provided to regulate the length of the grating and/or influence the birefringence of the fibre material. Controlled variation of the grating length and/or refractive index can be effected locally, for example by any of the techniques just mentioned, or over the whole of the fibre
15 length. The same or similar techniques could be applied to vary the birefringence of the fibre.

These and other techniques are well within the knowledge and capabilities of the average skilled man in the art and do not require dedicated description for the invention to be put into effect. However, for the avoidance of doubt, the following options are specifically mentioned as embodiments of the present invention. The fibre
20 may be tapered along its whole length. This improves the capacity for thermal adjustment of the required parameters.

An example is illustrated in Figures 3 and 4. The fibre 30 in Figure 3 is provided with a plurality of cores 31 as before. In this case, however, the fibre tapers in cross-section from one end to the other. The taper may be linear but it is not essential.
25 In Figure 4, a series of spaced heating elements 41 are provided along the length of the tapered fibre 40. The heating elements can be selectively energised to impose localised heating at selected parts of the fibre. In a further variation, a thermal gradient can be established over part or all of the length of the fibre, enabling thermal control
30 to be effected more precisely.

Alternatively, the fibre micro-holes can be filled with thermally sensitive material, such as polymer material, in order to create stressing rods by which control of

birefringence can be more readily achieved. In a yet further variation, the fibre itself may be constructed so that the fundamental mode of the fibre is designed to interact with the in-fill materials of the micro-holes to induce an electro-optic effect which alters the mode shape and therefore the birefringence of the fibre.

5 Any combination or permutation of any of the known techniques and those specifically mentioned above can be used to control both the grating and/or the birefringence of the fibre.

Where control is effected locally, compensation can be performed at the receive end and/or at the transmit end of a communication link incorporating a fibre in accordance with the invention. Similarly, where control is effected "globally", ie over 10 the whole length of the fibre, it can be initiated from either the transmit end and/or the receive end of the transmission link.

Control can be empirical or can be made automatic. As indicated schematically in Figure 5, a fibre 50 with birefringence control means 51, in accordance with 15 the invention, is coupled to a sensor 52 for sensing the difference in group velocity of the orthogonal polarisation states within the fibre. This difference signal is utilised in error signal generator 53 to generate an error signal. The error signal is used by the control means 51 to effect control of whatever compensation mechanism or technique or combination thereof is/are employed so as to counteract the sensed difference and 20 tend to reduce it to zero. In this sense, the invention provides an automatic equaliser adapted to compensate for polarisation mode dispersion in a fibre.

The invention is of particular benefit in that it, in its preferred embodiments, it is an all-optical, in-fibre compensation device that can be employed in optical fibre communication links, systems or networks to provide dynamic compensation for po- 25 larisation mode dispersion. The invention offers increased levels of control over and above existing methods and techniques.